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1 Description

2  
3 Method and device for determining a variable characteristic of  
4 a mass that rests on the seating area of a seat.

5  
6 The invention relates to a method and a device for determining  
7 a variable that is characteristic of a mass that rests on the  
8 seating area of a seat, especially one that is installed in a  
9 vehicle.

10  
11 In modern motor vehicles there is an increasing number of  
12 occupant restraint means, such as front airbags, side airbags,  
13 knee airbags and curtain airbags. Such occupant restraint  
14 means are designed to provide the best possible protection to  
15 the vehicle occupants in the event of an accident. This can be  
16 achieved in that the deployment area of the occupant restraint  
17 means is matched to the particular vehicle occupants in the  
18 vehicle. Therefore the risk of injury to babies or small  
19 children in the event of an accident can be less if the  
20 occupant restraint means do not deploy.

21  
22 Furthermore, the occupant restraint means should be activated  
23 in the event of an accident only where occupants are actually  
24 located, the risk of injury to whom is thus reduced. In this  
25 way, additional unnecessary high repair costs after an  
26 accident can be avoided. For these reasons, it is important to  
27 detect the occupancy of a seat of a motor vehicle by an  
28 occupant and also to classify these occupants with regard to  
29 their characteristics, e.g. with respect to body weight. In  
30 this respect, Crash Standard FMVSS 208 is receiving increasing  
31 attention. Compliance with it is demanded by numerous vehicle  
32 manufacturers. It specifies a classification of the respective  
33 vehicle occupants according to their weight, in order in the

1 event of a collision to adapt the control of an occupant  
2 restraint means suitably to the identified person as required.  
3 To determine the weight of an occupant it is known, for  
4 example, from DE 101 601 21 A1, to arrange pressure-sensitive  
5 sensor pads in a seating area of the seat and to determine the  
6 weight of the occupant from the measured signals from such  
7 seat sensor pads.

8  
9 From US 6,087,598, a weight detection device is known for  
10 determining the weight that bears on a vehicle seat of a motor  
11 vehicle. First to fourth force sensors are assigned to the  
12 vehicle seat, each of which detects forces that act on  
13 specific areas of the seating area. The first to fourth force  
14 sensors are connected in the area of an underside of the seat  
15 cushion underneath the seating area and are also connected to  
16 the chassis of the motor vehicle. They are arranged in such a  
17 way that they each determine the force acting on the seating  
18 area of the seat. In the event of an accident, occupant  
19 protection devices such as airbags, head airbags, side airbags  
20 or similar, are triggered depending on the measured signals  
21 from the sensors.

22  
23 Furthermore, it is known that an incorrect use of a vehicle  
24 seat to which at least one force sensor is assigned that  
25 detects the force in the area of the seating area of the seat  
26 can lead to a spurious measured signal. If such spurious  
27 nature of the measured signal remains undetected, this can  
28 lead to an incorrect classification of the occupant sitting on  
29 the seat. This then in turn means that in the event of an  
30 accident the occupant restraint means is not activated in a  
31 manner best suited to the particular occupant. Up until now  
32 the positions of the vehicle seat that gave rise to such an  
33 incorrect use was stated in the operating instructions.

1 However, this brings with it the danger that the occupant of  
2 the vehicle might not be aware of this statement in the  
3 operating instructions and thus be unaware of the dangers  
4 associated with such incorrect use of the vehicle seat.

5  
6 The object of the invention is to provide a method and a  
7 device for determining a variable that is characteristic of  
8 the mass resting on a seating area of a seat by means of which  
9 the reliability of the ascertained variable is determined.

10  
11 The object is achieved by the features of the independent  
12 claims. Advantageous developments of the invention are given  
13 in the subclaims.

14  
15 The invention is characterized by a method, with the following  
16 steps, and a corresponding device for determining a variable  
17 that is characteristic of a mass that rests on a seating area  
18 of a seat. An estimated value of the variable is determined  
19 depending upon at least one force that acts on the seating  
20 area and is detected by a force sensor. The estimated value is  
21 determined as reliable or unreliable depending on the  
22 oscillation behavior of the measured signal of the at least  
23 one force sensor.

24  
25 The invention is based on the knowledge that the oscillation  
26 behavior of the at least one force sensor is characteristic of  
27 the reliability of the estimated value of the variable. The  
28 oscillation behavior of the measured signal is caused by  
29 oscillations of the bodywork or movements of the occupants on  
30 the seat. If the position of the seat changes, so that the  
31 estimated value is no longer reliable, the oscillation of the  
32 measured signal also changes in a characteristic manner. No  
33 additional hardware expense, such as a further sensor, is

1 therefore necessary to determine whether the estimated value  
2 is reliable or unreliable.

3

4 According to an advantageous embodiment of the invention, the  
5 estimated value is determined as reliable or unreliable  
6 depending on a mass for the amplitude of the oscillations of  
7 the measured signal of at least one force sensor. The  
8 amplitude can be particularly simply determined and evaluated.  
9 A simple and precise detection as to whether the estimated  
10 value is reliable or not is thus enabled. In this respect, it  
11 can also be advantageous if only predetermined spectral areas  
12 of the oscillation of the measured signal are evaluated.

13

14 According to a further advantageous embodiment of the  
15 invention, the estimated value is determined as reliable or  
16 unreliable depending on a time duration of a predetermined  
17 change in the mass of the amplitude of the oscillation of the  
18 measured signal of at least one force sensor. By a suitable  
19 choice of time duration, any sporadic measuring errors in the  
20 measure signal of at least one force sensor can be eliminated,  
21 i.e. they do not lead to changes in the determination of  
22 whether the estimated value is reliable or unreliable.

23

24 According to a further advantageous embodiment of the  
25 invention, the measured signal of the force sensor is  
26 subjected to a Walsh transformation and the estimated value is  
27 determined to be reliable or unreliable depending on a measure  
28 for sequential contents of the Walsh transformed signal. The  
29 Walsh transformation is also known as a Walsh-Hadamard  
30 transformation. It is a discrete orthogonal transformation. It  
31 is related to the Fourier transformation. In contrast to the  
32 Fourier transformation that uses sine and cosine functions as  
33 basic functions from which the transformed signal is emulated,

1 the basic functions for the Walsh transformations are square-  
2 wave signals. The basic functions can only detect values +1  
3 and -1. By means of the Walsh transformation, a transformation  
4 of the time domain takes place in a sequential range. By  
5 transforming the measured signal of at least one force sensor  
6 using the Walsh transformation, the oscillation behavior of  
7 the measured signal can be simply analyzed, especially with  
8 appropriate simple computer hardware that does not have to be  
9 suitable for sine or cosine computing operations.

10  
11 In a further advantageous embodiment of the invention, the  
12 mass for the sequential content is formed by adding the  
13 amplitudes of predetermined sequences of the Walsh-transformed  
14 measured signal. This is particularly simple and a high  
15 correlation to the reliable or unreliable estimated value is  
16 obtained.

17  
18 A still more accurate determination of the reliability or  
19 unreliability of the estimated value of the variable can be  
20 easily achieved if the measured signals of several force  
21 sensors are subjected to the Walsh transformation and from  
22 these a monitoring value is determined for each measured  
23 signal and the estimated value is then determined as reliable  
24 or unreliable depending on the monitoring values.

25  
26 Exemplary embodiments of the invention are explained in the  
27 following with the aid of schematic drawings. The drawings are  
28 as follows:

29  
30 Figure 1 A seat 1 in a motor vehicle

31  
32 Figure 2 A force sensor  
33

Figure 3 A flow diagram of a program for determining a variable that is characteristic of a mass resting on a seating area of a seat

Elements with the same construction or function are identified by the same reference characters even when they occur in different illustrations.

A seat 1 is arranged in a vehicle. The seat has a seating area 2 and a backrest 4. A seat frame is formed in the seating area 2 that is connected by guide elements 5, 5a with a retaining device 6 and is thus secured in the vehicle. The retaining device 6 is preferably formed as a guide rail in which the seat 1 is guided and can thus slide along this guide rail. The position of the seat can thus, for example, be adjusted.

In the vehicle interior in which the seat 1 is located there is, for example a projection with an edge 7. The vehicle interior can also have a rear wall that has a further edge 8. If the seat is now slid correspondingly along the retaining device 6 it can, for example, come to a stop against the edge 7. It can also alternatively come to a stop against the other edge 8. In this case, for example, it can come to rest against its backrest 4 or also against another part of the seat such as the seat frame.

A first to fourth force sensor 9 - 12 is assigned to the seat 1. They are each mechanically connected to the retaining device 6 (Figure 2) by means of a connecting device 16 and also these first to fourth force sensors 9 - 12 are connected by the connecting device 16 to a leaf spring 18. The leaf spring 18 is connected at one end to the connecting device 16 and at the other end to a housing element 20. The housing

1 element 20 is attached to a reference device 22, that is  
2 preferably part of a chassis of the vehicle. Furthermore, a  
3 limiting element 24, that serves as an overload protection in  
4 the compression and tension directions with respect to force  
5 introduced in the direction shown by the arrow 32, is assigned  
6 to the first to fourth force sensor 9 - 12. A sensor element  
7 26, that for example can detect a deflection of the leaf  
8 spring 18 either inductively or capacitively and the measured  
9 signal of which is thus representative of the force acting on  
10 the leaf spring 18 and thus of the force acting on the  
11 retaining device 6, is assigned to the connecting device 16.

12  
13 As an alternative, the force sensors 9 - 12 can also be  
14 suitably arranged directly in the seat, for example between  
15 the seat frame and the guide elements 5, 5a.

16  
17 The force sensors 9 - 12 are arranged so that each individual  
18 force sensor detects the force that acts on it in the area in  
19 one of the corners of the seating area 2. The force sensors 9  
20 - 12 can also be otherwise formed and arranged. Furthermore,  
21 there can be just one, or two, three or more than four force  
22 sensors used.

23  
24 A control device 28 is provided that is designed to determine  
25 the variable that is characteristic of the mass that rests on  
26 the seating area 2 of the seat 1 and thus can also be regarded  
27 as a device for determining the variable that is  
28 characteristic of the mass that rests on the seating area of  
29 the seat. It is furthermore preferably designed to determine a  
30 control signal for the firing unit 30 of an airbag, that is  
31 assigned to the seat 1 and is therefore an occupant restraint  
32 means.

33

1 A program for determining the variable that is characteristic  
2 of the mass that rests on the seating area of the seat is  
3 stored in the control unit 28 and is processed in the control  
4 unit 28 during the operation of the vehicle. The program is  
5 explained in more detail in the following with the aid of the  
6 flow diagram in Figure 3. The program is started at step S1 in  
7 which variables are initialized as required. Thus, for  
8 example, a counter CTR can be initialized. The start  
9 preferably takes place close to the time the engine of the  
10 motor vehicle starts.

11  
12 In a step S2, measured signals MS1, MS2, MS3, MS4 of the first  
13 to fourth force sensor 9 - 12 are detected at corresponding  
14 discrete time points  $t_0 - t_n$ . For example,  $t_n$  has a value  $t_7$ ,  
15 i.e. eight values of the respective measuring signal MS1 - MS4  
16 are detected.

17  
18 Then, in step S4 a weight G that is characteristic of the mass  
19 resting on the seating area 2 of the seat 1 is determined. The  
20 weight G is determined depending on the measured signals MS1 -  
21 MS4 of the first to fourth force sensors 9 - 12. This can be  
22 achieved very simply by adding a measured value of the first  
23 to fourth measured signal MS1 - MS4 in each case.

24  
25 Alternatively, the mass resting on the seating area 2 can, for  
26 example, also be directly determined in step S4.

27  
28 In a succeeding step S6, the measured signals are subjected to  
29 a Walsh transformation and thus transformed from the time  
30 domain to the Walsh-transformed sequence domain. The  
31 corresponding sequences s are designated with  $s_0 - s_n$ . The  
32 Walsh transformation is a mapping associated with the Fourier  
33 transformation. The basic function of the Walsh transformation



1 is a Boolean function. It can only take the values 1 and -1.  
2 The Walsh transformation takes place by multiplying the  
3 measured signal vector formed by the measuring signal values  
4 with the Hadamard matrix. An example of the Hadamard matrix  
5 for a Walsh transformation with a measured signal vector with  
6 eight discrete measured signal values is shown in block B1.  
7 The multiplication takes place by lines. The individual lines  
8 of the Hadamard matrix according to block B1 are shown in  
9 signal form by way of example. The zeroed sequence  $s_0$  of the  
10 respective Walsh transformed represents its steady component.  
11 The first sequence  $s_1$  represents the fundamental oscillation.  
12 The other sequences  $s_2 - s_n$  represent harmonics.  
13  
14 In a step S8, a first monitoring value  $UW_1$  is then determined  
15 by summing the amplitudes  $A$  of the transformed measured signal  
16  $MS_1$  of the first force sensor 9 over its sequences  $s_1 - s_n$ .  
17 Alternatively, the sum can also be formed using only selected  
18 sequences  $s$ , that are suitably chosen and particularly  
19 characteristic of the reliability or unreliability of the  
20 weight  $G$  determined in step S4. Furthermore, in step S8  
21 further corresponding second, third and fourth monitoring  
22 values  $KW_1 - KW_4$  are determined by summing corresponding  
23 amplitudes of the sequences  $s$  of the second to fourth measured  
24 signals  $MS_2, MS_3, MS_4$ .  
25  
26 In a step S9, a monitoring value is determined depending on  
27 the first to fourth monitoring values  $UW_1 - UW_4$ . This can take  
28 place either weighted or by a simple summing of the first to  
29 fourth monitoring values  $UW_1 - UW_4$ .  
30  
31 In a step S10, a check is carried out to determine whether the  
32 monitoring value  $UW$  is less than a specified first threshold  
33 value  $SW_1$ . The specified first threshold value  $SW_1$  is

1 preferably determined by corresponding tests on a vehicle or  
2 by simulation, and in such a way that if it is undershot by  
3 monitoring value UW there is a high probability that the  
4 weight G determined in step S4 is not reliable. This can be  
5 due to the fact that the seat 1 is, for example, resting  
6 against the edge 7 or other edge 8 or is tilted against it.  
7 The consequence of this is that the introduction of the force  
8 from the seating area 2 to the force sensors 9 - 12 is changed  
9 and thus the respective measured signal of the first to fourth  
10 force sensors 9 - 12 has a changed characteristic.

11  
12 If the condition of step S10 is not fulfilled, the counter CTR  
13 is decremented in step S12 by a predetermined value, that can  
14 for example be 1. Alternative, the counter can also be reset  
15 to its initialization value.

16  
17 If on the other hand, the condition of step S10 is fulfilled,  
18 the counter CTR is incremented in step S14 by a predetermined  
19 value, that can for example be 1.

20  
21 In step S16, a check is then carried out to determine whether  
22 the counter CTR is greater than a second threshold value SW2,  
23 that is permanently specified. If this is not the case, a  
24 logic variable LV is given a reliability value ZU in step S18.  
25 If on the other hand, the condition of step S16 is met, the  
26 logic variable LV is provided with an unreliability value NZU  
27 in step S20.

28  
29 If the logic variable LV is provided with an unreliability  
30 value NZU, this can, for example, be signaled to the driver of  
31 the vehicle, for instance acoustically or visually, and the  
32 driver can be requested to move the seat to a different  
33 position. Alternatively, or in addition, an entry that can be

1 evaluated after an accident if required can be entered in a  
2 memory in which operating data is stored.

3  
4 Following steps S12, S18 and S20, the program is continued in  
5 a step S13 in which it dwells for a predetermined waiting time  
6  $T_W$  before step S2 is again processed. The waiting time  
7 duration  $T_W$  is furthermore suitably chosen so that step S2  
8 and the succeeding steps are processed at a predetermined  
9 frequency during the operation of the vehicle.

10  
11 Alternatively, fewer than all the measured signals MS1 - MS4  
12 of the first to fourth force sensors 9 - 12 can also be  
13 detected in step S2, for example only measuring signal MS1 of  
14 the first force sensor 9. Correspondingly, the weight G can  
15 then be determined in step S4 only depending on the measured  
16 signals MS1 - MS4 determined in step S2. Furthermore,  
17 regardless of steps S2 and S4 fewer than the first to fourth  
18 measured signals MS1 - MS4 can be subjected to a Walsh  
19 transformation in step S6, for example, only the measured  
20 signal MS1 that is assigned to the first force sensor 9.  
21 Therefore only a corresponding determination of the relative  
22 monitoring value UW1 is determined in step S8 and step S9 is  
23 then adapted accordingly.

24